***Comparative evaluation of power generating capacity of a low head river using conventional small hydropower and hydrokinetic turbines using Ona River, Ibadan, Oyo State, Nigeria a case study***

**ABSTRACT**

Considerable amount of the global electricity production is obtained from hydropower but with insignificant contribution from low head rivers (i.e. ≤ 5m). The interests among researchers towards exploring and harnessing energy from low head hydro resource is gaining more prominence in the recent years. Therefore, this study was designed to investigate the competitiveness of the hydrokinetic turbine (HKT) against conventional hydro turbine for harnessing the hydropower available in low head rivers. A vertical axis hydrokinetic turbine using NACA 0021 airfoil profile and a cross-flow turbine were the technologies employed for the study. Hydrological data were collected from Ona River in Ibadan, Nigeria. The data were used as input for computer simulation.in respect of the two hydropower generation technologies considered in this study. The simulation results were used to develop a score card for evaluation of the two technologies. This study revealed that HKT is more suitable for a zero or low head river than a conventional hydro-turbine such as cross flow turbine.

**Keywords**: Hydrokinetic; Hydropower; Turbine; Low Head and Ona River

1. **INTRODUCTION**

Without mincing words, energy remain the life wire of socio-economic growth and development across the globe. The demand for electricity is growing rapidly around the world as economic development spreads to emerging economies (Yüksel, 2007). It has been reported that nearly 1.4 billion people worldwide do not have access to electricity; while about 85% of them are from rural communities (Kaygusuz, 2007 and Lata-Garcia et al., 2018). Renewable energy resources are gaining global attention due to depleting fossil fuels and their harmful environmental effects associated with emission of Green House Gases (GHG) have made it imperative to consider alternative ways in which affordable, clean and readily available energy sources can be harnessed (Singal and Saini ,2007; Kolekar et al., 2013 and Akinyemi et al., 2015).

Among hydro, wind, solar, biomass and geothermal energies; hydro power can be considered as the most exciting and sustainable renewable energy resource for electricity generation (Altnbilek, 2005, Akorede et al, 2010; Kolekar et al., 2013) providing 19% of the planet’s electricity (Paris 2002; Rahman et al., 2017). The interest of researchers in small hydropower (SHP) development (Yanmaz, 2007; Abbasi and Abbasi, 2011; Sachdev et al., 2015;) and hydrokinetic (HKT) technology (Kumar and Saini.2014; Kumar and Pandey, 2017), for power production using ‘zero head’ turbines is growing tremendously. The authors describe hydrokinetic resource as small hydro energy generation and it is a recently developed turbine technology which makes use of kinetic energy from flowing river, tidal and water streams to generate electricity.

Some research efforts on hydrokinetic for electricity generation have been reported. Ismail and Batalha (2015) studied the hydrokinetic turbines blade profiles of a river in Brazil. Four blade profiles were investigated. Computational Fluid Dynamic (CFD) simulations showed that circular arc profiles are more efficient and produce more power. The work of Els and Junior (2015) considered evolution of the hydrokinetic technology for rural electrification in Brazil. Attempt was made by the authors on integrating hydrokinetic electricity generated into national grid. Salau et al (2017) carried out hydrokinetic power estimation in selected rural communities in Oke Ogun, Nigeria. At a head of 0.3 metres, the authors estimated 36.4 MW as the total theoretical hydrokinetic power potential for the ten (10) basin considered in the study. Some other research works have also been documented (Ruopp et al., 2014; Gunawan et al., 2015; Niebuhr et al., 2018).

With respect to low or no heads hydro resources, research concerns are shifting from the conventional Small hydro power (SHP) scheme with run of water to hydrokinetic turbine technology where run of water is not required (Chica and Perez 2015; Bir et al. 2011; Adejumobi et al. 2013; Kusakana, 2015). Notwithstanding, in-depth literature review shows that the available experimental data for deployment of hydrokinetic in west Africa countries such as Nigeria is not robust. Therefore, this research was designed to investigate the competitiveness of HKT over conventional SHP scheme by evaluating their power generating potential from low head river using River Ona in Ibadan Nigeria as a case study.

1. **BACKGROUND** 
   1. **Demand for Low Head Turbine Technology**

Hydropower, large and small, remains by far the most important of the renewables for electrical power production worldwide (Ramachandra and Shruthi, 2007). The water resources in the low head category are the ones with the heads less than ten metres (Mosonyi, 1988; Hall,.2004). Senior (2009) revealed that that much of the world's available hydropower potential has already been utilized, hence there is need to focus attention on hydropower sites with very low head differences which are sites with vertical distances through which water falls is less than 5 metres. Figure 1 shows the demand side of hydropower technology is the one that can derive significant power output from low head water resources.

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**Figure 1:** Established Hydropower Machines and Demand for New Technology (Senior, 2009)

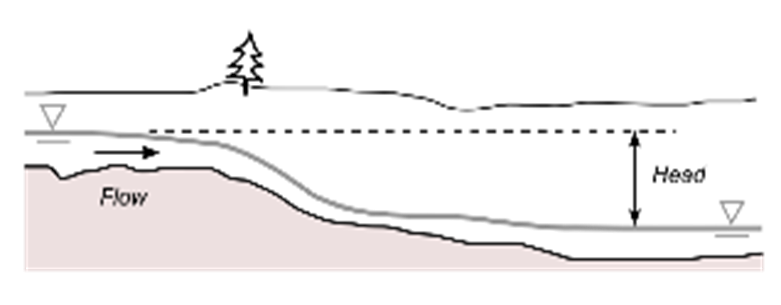
The low head poses a challenge to power generation through the conventional small hydropower system but the emergence of the hydrokinetic technology has facilitated the means to harness hydropower in flowing water bodies with or without head. However HKT is yet to be well established and several researches have been done and still in progress towards improving the technology (Fo, 2003; Laws and Epps 2016; Vermaak et al. 2014) .

* 1. **Conventional SHP**

Conventional hydro-turbines convert water pressure into mechanical shaft power, which can be used to drive an electricity generator, or other machinery (Paish, 2002; Purohit, 2008). The power available is proportional to the product of pressure head and volume flow rate (Ramachandra and Shruthi, 2007; Kaldellis et al. 2001). The general formula for any hydro system’s power output is:

1

where *P* is the mechanical power produced at the turbine shaft (Watts), h is the hydraulic efficiency of the turbine, *ρ* is the density of water (kg/m3), *g* is the acceleration due to gravity (m/s2), *Q* is the volume flow rate passing through the turbine (m3/s), and has demonstrated in Figure 2is the effective pressure head (m) of water across the turbine



**Figure 2** Hydro Power Basics (Paish, 2002)

* 1. **Hydrokinetic Turbine Technology**

The function of hydrokinetic turbines is to capture the kinetic energy of flowing water current and transfer it into a shaft. Hydrokinetic turbines can only capture a fraction of the kinetic energy in the water that pass through its cross section. The fraction is known as power coefficient, Cp (Tewari et al. 2015; Bustamante et al. 2015; Rumpfkeil et al. 2015) . The power captured by a hydrokinetic turbine can be expressed as:

2

Similar to wind turbines, the power coefficient, Cp, of a hydrokinetic turbine depends on Tip-Speed Ratio. By definition, Tip-Speed Ratio (TSR) λ is the ratio of the speed of the blade, at its tip, to the speed of the flowing water (Jones, 1950; Rumpfkeil et al., 2015).. The formula for TSR is as shown in equation 3.

3

The relation between TSR and power coefficient Cp can be understood intuitively. If the turbine’s blades spin too slowly, then most of the water will pass through the rotor without being captured by the blades. However, if the turbine spins too fast, then the blades will always travel through used, turbulent water. There must be enough time lapses between two blades travelling through the same location so that new water can enter and the next blade can harness the power from that new water, not the used, turbulent water (Riegler, 1983)

1. **MATERIALS AND METHOD**
   1. **Site Selection and Hydrological Data Collection**

The selected source of water for this work is River Ona in Ibadan, located inside University of Ibadan, Oyo State, Nigeria as shown in figure 3.

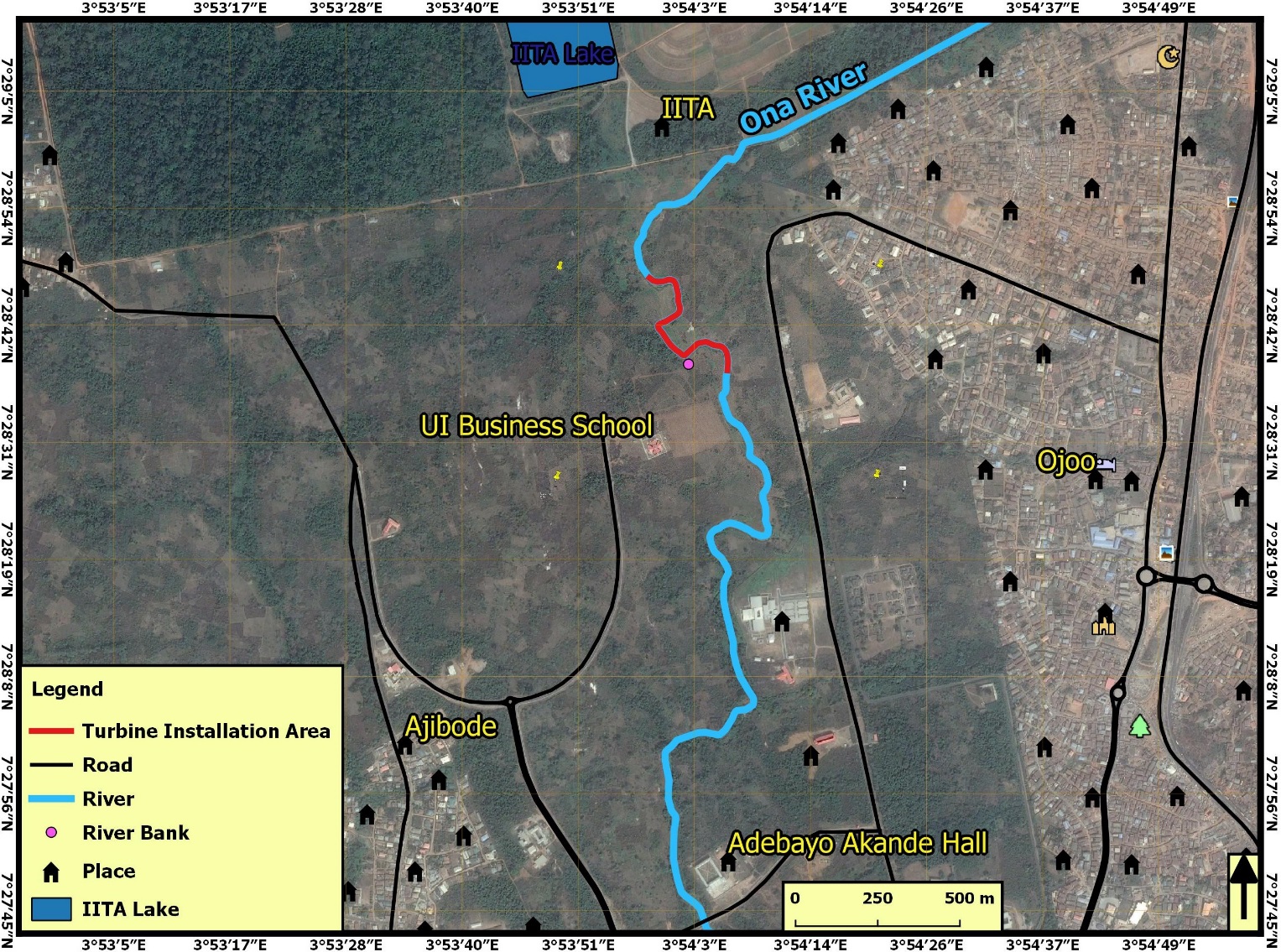


Figure 3. Aerial View of Ona River (Google earth)

A critical starting point in SHP development is the estimation of the power potential of a proposed site. Every other key component of the scheme such as turbine selection and sizing depend on the estimated power potential of the site. The hydrological data collected at the site were elevations (m) at various points along the river to determine the head (m) of the river and velocity (m/s) of the river and flow (m3/s). Figure 4 showed the site visit and survey activities. The power potential was calculated for conventional SHP and hydrokinetic turbine schemes for River Ona using hydrological data collected during site visit. This was used for the preliminary designs for both technologies for the purpose of comparative evaluation.

Figure 4: Taking hydrological data at Ona River

* 1. **Design of Cross Flow Turbine (Conventional SHP)**

The set of mathematical equations used in the design steps for cross flow turbine in Nasir (2013) was used and computed using MATLAB. The mathematical equations used are as follows:

**(a) Turbine Power (Pt) in Watt**

The electrical power of the turbine in Watt was determined with the equation 4 using the data gathered on the field as inputs:

4

where,

ρ = the water density (1000 kg/m3),

g = the acceleration due to gravity (9.81 m/s2)

Hn = Net head (m)

Q = Flow rate (m3/s)

**(b) Turbine Efficiency (ηt):**

where,

C = Nozzle roughness coefficient

ψ = Blade roughness coefficient

α = angle of attack (o)

Mockmore and Merryfield (1949) revealed that angle of attack (α) should be kept as small as possible and stated (16o) can be obtained without much inconvenience.

**(c) Turbine Speed (N):**

6

**(d) Runner Outer Diameter (Do)**

7

**(e)** **Calculation of Blade Spacing (tb):**

8

**(f) Radial Rim Width (a):**

9

**(g) Runner Blade Number (n):**

10

**(h) Water Jet Thickness (tj):**

11

**(i) Runner Length, L (m):**

12

**(j) Distance between Water Jet and the Center of Runner Shaft (y1):**

13

**(k) Distance between Water Jet and the Center of Inner Periphery Runner Shaft (y2):**

14

**(l) Diameter of the Runner**

15

**(m) Radius Blade Curvature, Rc (m)**

16

* 1. **Design of Hydrokinetic Turbine**

Below are the governing equations used for the preliminary design of hydrokinetic turbine using NACA0021 hydrofoil as stated in Khan et al. (2009); Kolekar (2013); Liu (2014); Kolekar and Banerjee (2015) :

17

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where

𝜆 = Tip Speed Ratio (i.e. the ratio of blade tip speed to fluid speed)

At = Cross sectional area turbine flows through

CP = power coefficient

Ct = turbine coefficient

ωt = Turbine rotational speed (rad/s)

R*t* = radius of turbine (m)

Ww = flow speed of water (m/s)

σ = solidity (σ) that is defined as the ratio of blade chord length times the number of blades to turbine circumference.

B = number of turbine blade

c = length of blade cord

Re = Reynold number

ρ = density

μ = dynamic viscosity of water (Pa.s)

* 1. **Comparative Evaluation of the two technologies**

The two technologies; cross flow turbine for conventional SHP and hydrokinetic turbine design parameters were compared for the purpose of evaluating their power generating potential using Ona River hydrological data as a case study under various boundary conditions and scenarios. A scorecard Matrix was developed with the following as the major evaluation criteria:

* The technically feasible power output
* Ease and Cost of fabrication
* Scalability
* Cost benefit analysis
* Ease of technology transfer

1. **RESULTS AND DISCUSSION**

**4.1 Hydrological Data**

Table 1 shows the hydrological data collected at Ona River which were major input for the preliminary design of the two SHP technologies under evaluation.

**Table 1:** Hydrological Data for Ona River

|  |  |
| --- | --- |
| DESCRIPTION | **DATA** |
| Location | Stream along Ona River behind UI School of Business, U.I. |
| Coordinates | 7° 28′ 38.6″ N  3° 54′ 2.3″E |
| Gross Head (Hg) | 2m |
| Water Velocity (vw) | 0.1m/s |
| Flow rate (Q) | 0.95839 m3/s |
| Maximum Depth | 0.5 m |
| Average Width | 9 m |

**4.2 Power Outputs**

As observed in the hydrological data the river has a very low head of 2 m and low velocity of about 0.1 m/s. This makes the river practically difficult to be utilised for power generation at its present state with conventional SHP and the river may require some kind of a dam that creates an artificial water head, which should be large enough to propel a water turbine (Fleisinger et al. 2014). For HKT to be utilized the stream velocity will also require to be increased which can be achieved through channel augmentation (Vermaak et al. 2014; Ait-mohammed et al. 2014; Mukherji 2010)

The predicted potential power output for the two SHP technologies was based on the possibility of creating artificial head to achieve higher head and augmenting the flow channel to increase higher stream velocity in the case of conventional SHP and hydrokinetic turbine respectively.

Figures 5 and 6 show that how the simulated power outputs vary with the increase in head and velocity of the stream in the case of conventional SHP and hydrokinetic turbine technology respectively. The values obtained for the maximum possible power outputs were 56 kW at 6 m Head and 400 kW at 3m/s for conventional SHP and hydrokinetic turbine technology, respectively.

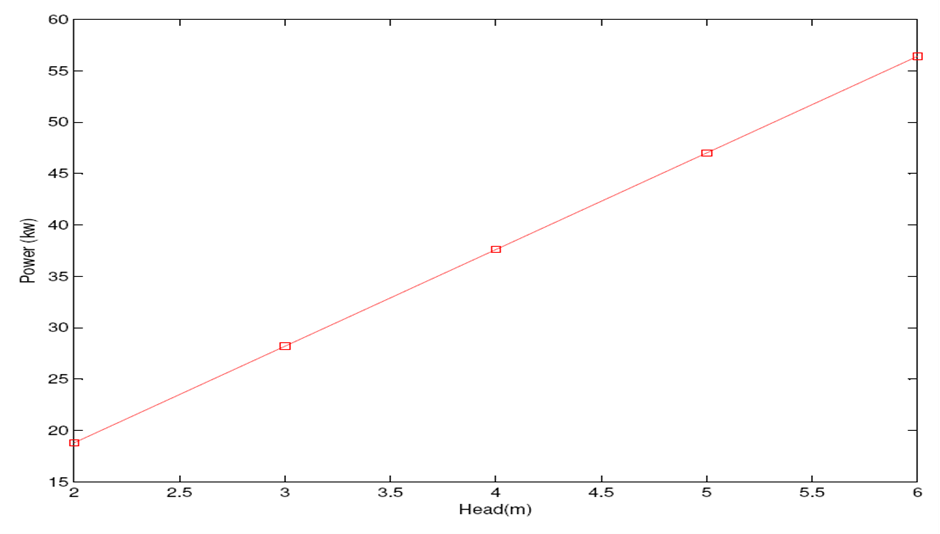


Figure 5: Variation of Power Output of Cross Flow Turbine with increase in Head (m) of the river

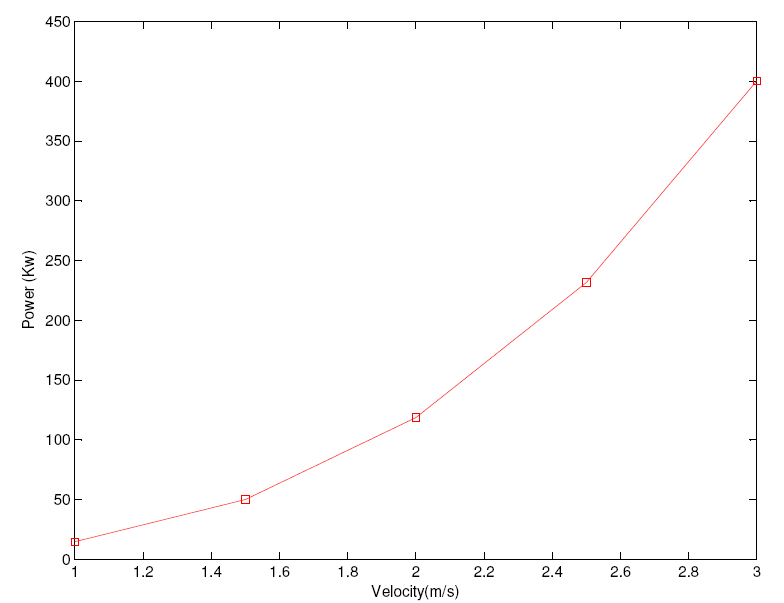


Figure 6: Variation of Estimated Power Output of Hydrokinetic Turbine with increase in Velocity of the river

**4.3 Design Parameters for Cross Flow turbine**

Tables 2shows the simulated design parameters for cross flow turbine for power output ranging from 18 – 47 kW.

The design parameters indicate dimensions of the components of the mechanical part of the turbine. Figure 7 shows the components of a typical cross flow turbine

**Table 2:** Design Parameters for Cross flow Turbine at Various Heads

|  |  |  |  |  |
| --- | --- | --- | --- | --- |
| HEAD (m) | **2** | **3** | **4** | **5** |
| Power (Kw) | 18.80 | 28.21 | 37.61 | 47.01 |
| Turbine efficiency (%) | 70 | 70 | 70 | 70 |
| Runner speed (rpm) | 325 | 359 | 386 | 407 |
| Length of runner (m) | 10.2 | 15.3 | 20.3 | 25.4 |
| Number of blade | 18 | 18 | 18 | 18 |
| Runner outer diameter(m) | 0.034 | 0.041 | 0.048 | 0.054 |
| Runner inner diameter(m) | 0.127 | 0.155 | 0.179 | 0.2 |
| Blade spacing (m) | 0.034 | 0.041 | 0.048 | 0.054 |
| Water jet thickness (m) | 0.056 | 0.069 | 0.08 | 0.089 |
| Distance between water jet and shaft centre | 0.023 | 0.028 | 0.032 | 0.036 |
| Distance between water jet and inner periphery of runner (m) | 0.01 | 0.012 | 0.014 | 0.015 |
| Radius of blade curvature (m) | 0.032 | 0.039 | 0.049 | 0.05 |



Figure 7: Components of typical cross flow turbine (Nasir,2013)

**4.4 Design Parameters for HKT**

Tables 3 show the simulated design parameters for 50 kW HKT turbine. The design parameters indicate dimensions of the components of the mechanical parts of the turbine. Figure 8 shows the components of a typical HKT turbine

**Table 3.** Design Parameters for Hydrokinetic Turbine

|  |  |
| --- | --- |
| **Parameters** | **Values** |
| Expected Power | 50 Kw |
| Water Velocity | 3 m/s |
| Radius | 3.1 m |
| Height of the Blade | 1.4 m |
| No of Blade | 3 |
| Tip Blade Ratio | 4 |
| Blade Hydrofoil Model | NACA 0021 |
| Turbine Rotational Speed | 371 rpm |
| Turbine Angular Velocity | 3.94rad/s |
| Turbine Torque | 12.68 Nm |

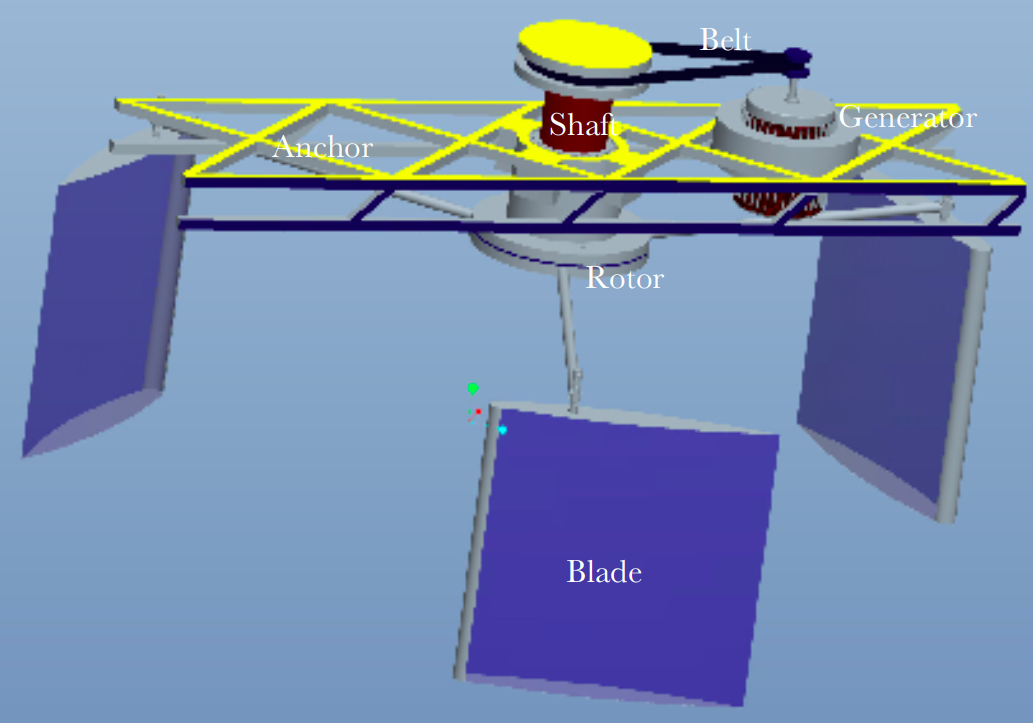


Figure 8: Conceptual design of Vertical Hydrokinetic

**4.5 Technology Evaluation**

The main objective of this work is to conduct a comparative evaluation of the two SHP technologies earlier mentioned in order to justify the choice of hydrokinetic turbine technology over the conventional small hydropower scheme. Table 4 shows technology evaluation selection matrix with a set of criteria to enable select the best technology for a SHP scheme suitable for the proposed site. The table clearly shows that hydrokinetic turbine technology is a better option than cross flow turbine technology.

**Table 4:** Technology Selection Criteria Scorecard

|  |  |  |  |
| --- | --- | --- | --- |
| S/N | **Criteria** | **Cross Flow Turbine Technology** | **Hydro Kinetic Turbine** |
| 1 | Technically Feasible Power Output | 1 | 2 |
| 2 | Cost of Fabrication | 1 | 2 |
| 3 | Ease of Fabrication | 1 | 2 |
| 4 | Ease of Installation | 1 | 2 |
| 5 | Modularity | 1 | 2 |
| 6 | Scalability | 1 | 2 |
| 7 | Maintenance and Serviceability | 2 | 1 |
| 8 | Amount of Civil Work | 1 | 2 |
|  | Overall Score | 9 | 15 |
|  | NOTE:  2 = Comparatively Higher or Better  1 = Comparatively Lower or Worse |  |  |

1. **CONCLUSION**

The preliminary investigation in this research entailed the development of MATLAB code for modeling of both conventional Small Hydro Power (SHP) and Hydrokinetic Turbine (HKT) for the purpose of justifying the choice of more suitable technology for the water resources with or without head using hydrological data for Ona river as a case study. The findings of this research revealed the advantage of HKT technology over the conventional SHP technology for low or zero head water resources in terms of technically feasible power output, manufacturability, modularity and scalability. Further research works are required to explore more opportunities associated with the advent of this HKT technology.

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