

DEVELOPMENT OF ALUMINIUM BOILING POT INCORPORATED WITH FRACTALLY GENERATED INTERNAL CYLINDRICAL FINS

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ABSTRACT

Aluminium boiling pots as typical in heated liquid-filled vessels are indispensable for heating purposes especially for domestic water boiling. Available information on its current design showed that it required prolonged heating duration, leading to high consumption of fuel such as Liquefied Petroleum Gas (LPG). Internal cylindrical fins are used in heated liquid-vessels, but with limited heat transfer enhancement. Fractal induced surfaces being self-similar geometrical-objects have high potential for heat transfer enhancement, but there is dearth of information in their use for aluminium boiling pot's integrated with internal cylindrical fins. Therefore, a 7-litre Experimental Aluminium Boiling Pot (EABP) and internal cylindrical fins ($\text{Ø}5 \times 140$ mm) were designed and fabricated in this study. The EABP had base-thickness, height, internal-diameter and external-diameter of 10, 155, 258 and 274 mm, respectively and 121 fractal placement locations for the internal cylindrical fins. The pot performance when filled with liquid and containing selected number of internal cylindrical fins placed according to affine rules can be evaluated for arbitrary Iterated Fractal System (IFS).

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Keywords: Aluminium boiling pot, Fractal objects, Internal cylindrical fins, Heat transfer enhancement

1.0 Introduction

Without cookware, humans cannot easily heat water and cook their foods. Pots are used in almost all households, kitchens and restaurants for heating water and to prepare various meals (Guma and Uche, 2019a). Aluminium pots are commonly used cookware because of their ability to heat and cool more quickly, light-weight and fair strength, excellent corrosion resistance, low cost due to availability of raw materials, ease to be fabricated, formed and machined, unsurpassable recyclability and casting properties of the raw materials, durability, etc, compared to most other food-grade metal containers (Guma and Durami, 2019).

Foundry technology is one of the vital bases for rapid industrial development of any nation. Sand casting is the most versatile, widely used and important method of casting and accounts to about 70 % of all foundry products (Guma, 2010; Guma, 2012; Ogboi, 2018; Guma and Ogboi, 2019). Metals that can be sand-cast include ferrous metals such as steel, cast iron and many non-ferrous metals, but aluminium is the most commonly used metal in the metal casting industries due to its comparatively far more properties of casting merit than other metals (Guma and Uche, 2019b).

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Over the years, many interesting studies have been done in improving cook stove efficiency. Khan and Saxena (2013) used several burner head designs to study how well an LPG cooking stove performed. Ali (2014) conducted performance tests on a home LPG stove using a conventional burner and porous material. Obada *et al.* (2014) designed and built burner system that runs on biogas. The parametric research of gas burners with high efficiency and minimal emissions was the focus of Hou and Chou (2013). Anafi *et al.* (2018) developed a low-cost pressurized kerosene stove. The pressured kerosene stove outperformed the traditional kerosene stove (wick stove) in terms of heat generation and carbon soot production, according to the findings of their performance test. The performance and emission characteristics of the pongamia oil-kerosene blend used in commercial kerosene stoves were studied by Shetty *et al.* (2015). An enhanced charcoal cooking stove was designed, manufactured, and its performance evaluated by Komolafe and Awogbemi (2010). Masekamani *et al.* (2015) examined the emissions and thermal performance of three liquid fuel stoves- a kerosene stove, an ethanol gel stove, and a prototype methanol stove. Varun *et al.* (2018) used waste cooking oil – kerosene blends to study the efficiency and emission properties of commercial kerosene stoves. Tesfay *et al.* (2024) compared the performance of three recently created biomass stove prototypes with conventional and Mirt stoves.

One of the most crucial aspects of fuel conservation is the water boiling pot's contact surface with the flame. The pot itself has an improved thermal efficiency because of its design and unobstructed heat transfer capabilities. In order to minimize wasted flames escaping through the pot's edges, the flame beneath the water boiling pot should be in direct contact with the pot itself. This reduces efficiency because excess flame that rises above the pot skirt's size is lost to the atmosphere. The round-bottomed pots are more stable because of their lower center of gravity. The use of flat-bottom pots, which became widespread due to European influence, is prevalent in many locations these days (Singh and Sahu, 2017). WHO (2008) defined efficiency as the sum of heat transfer efficiency and combustion efficiency. Heat transfer efficiency may be significantly influenced by the shape of the pot bottom. The concept that a flat-bottom pot is a "standard pot" stems from the fact that most writers examined stove efficiency but did not conduct many trials with water boiling pots. The geometry of the pot and the relationship between pot design and heat transfer efficiency were not expressly addressed by Baldwin (1987) when he discussed pot efficiency.

Singh and Sahu (2017) enhanced the boiling heat transfer of pots by redesigning the pots' bottom surface through surface modification with flue tube arrangement. The authors compared the thermal efficiency of three different modified bottom surfaces with flue tubes to those of a conventional flat bottom pot. According to this research, the boiling pot with flue tube modified bottom produced an efficiency that was 9-10 % greater than the pot with a flat bottom. It was further revealed from their study that boiling point is reached earlier in modified bottom pot with flue tube compared to other pots. Singh and Sahu (2018) also corroborated the earlier study of Singh and Sahu (2017) through the use of boiling pots with modified bottom surfaces made of vertical tubes. According to their results, boiling pots with modified bottom surfaces made of vertical tubes had an efficiency that was 25-29 % higher than pots with an unaltered flat bottom. Additionally, their findings demonstrated that the boiling point is achieved faster in modified pots than in unaltered pot.

Wang *et al.* (2022) also enhanced the boiling heat transfer ability of cookware through surface modification by the addition of fins on the base of the wok and observed that when 42 fins are considered for the study, overall efficiency of cookware is enhanced by approximately 8 % compared to the basic cookware that lacks this kind of heat exchange. Naphon (2014) carried out the thermal efficiency of fabricated domestic cooking pots modified with spirally twisted tape and with or without insulation. The author's results obtained from the modified cooking pot compared with those from the standard cooking pots. It was found that the modified cooking pot required 15-20 % less energy than the standard cooking pot to bring water to boiling.

The heat conductivity of a locally manufactured cast aluminum pot was analyzed by Fierkwap and Ilouno (2021). According to the authors' investigation, the kind and composition of materials used to make a pot can affect its thermal characteristics. Cast aluminum pots have different thermal qualities from one another. 162.36 W/m/K was found to be the average thermal conductivity of the cast aluminum pots. This suggests that it will conduct more heat through its layer and that food and water will not often react with it. The authors also disclosed that, in comparison to other pots, cast aluminum pots have a reasonably high thermal conductivity, which saves a significant amount of time during cooking and water heating.

The impacts of fractal surface geometries and boundaries have been a topic of interest for fractal study in engineering. It has proven possible to organise an object's conductivity by arranging fractal patterns. Kacimov and Obnosov (2000) found that by organising distinct materials with

different thermal conductivities using a Sierpinski carpet pattern, the overall thermal conductivity may be changed to suit needs. According to Adrover (2010), the surface fractal dimension has a significant impact on the thermal boundary layer for convection; surfaces with a higher fractal dimension transport more heat. Anton (2017) conducted a study on the thermal efficiency of a double-pipe heat exchanger with a Koch snowflake fractal pattern. Several heat transfer enhancement techniques can be applied to double-pipe heat exchangers to increase their efficacy. In particular, the Koch snowflake fractal pattern was included into the cross-section of a heat exchanger's inner pipe. The heat exchanger's surface area increased when the Koch snowflake fractal pattern was used. Based on the study, it was discovered when compared to a conventional double-pipe heat exchanger with a circular cross-section; a double-pipe heat exchanger with a cross-section in line with the second iteration of the Koch snowflake fractal pattern produced an increase in the overall heat transfer coefficient and heat transfer rate of 18 % and 75 %, respectively.

Guo *et al.* (2024) conducted an experimental study on the use of fractal fins to enhance heat transfer of phase change materials. The authors created and produced fractal fins modeled after plant leaves to increase the phase change unit's heat charging capacity. Their findings demonstrated that fractal fins have superior heat transfer enhancement effects compared to rectangular fins because the enhancement of heat conduction surpasses the suppression of natural convection. Oskouei *et al.* (2023) used the Fibonacci sequence as the basis for their fin design. In comparison to conventional longitudinal fins, experimental and numerical results demonstrate that this fin's total melting time of latent heat thermal energy storage is shortened by 20%, solidification speed is increased by 45%, and the temperature distribution is more uniform due to the secondary flow produced by the Fibonacci fins. Jiang *et al.* (2023) used numerical simulation to examine how the melting process in the rectangular phase change unit was affected by various position ratios, length ratios, and fin counts of tree-like fins. Zhang *et al.* (2022) created a fin that was modeled after snowflakes and conducted experiments to compare units with the same volume fraction that had longitudinal fins, no fins, and snowflake fins. The melting and solidification durations of units with snowflake fins can be shortened by 32.23% and 51.81%, respectively, as compared to longitudinal fins. Snowflake fins are also clearly more advantageous for the process of heat discharge.

The impact of combining various fractal fins on the melting process was examined by Luo *et al.* (2022). Numerical simulation was used to compare the effects of the fins' distance from one another, their heat transfer area, and their combination on the fins' thermal characteristics. According to the findings, the composite fractal fin heat exchanger's phase change materials' total melting time is up to 68% less than that of the traditional fractal fin heat exchanger. Through numerical simulations and experiments, Shi *et al.* (2022) examined the impact of the fractal fins' length, width, and bifurcation angle on the enhancement of heat transfer in a double-channel finned tube. They also examined the melting processes when the two tubes were in different operating states for heat charging and discharging. Using spider webs as inspiration, Wu *et al.* (2020) created mesh fins that enhanced solidification performance and reduced the total solidification time by 47.9% when compared to longitudinal fins of the same volume. Despite the potential of fractals for heat transfer enhancement, the scholarly discourse remains scant, particularly regarding their use in aluminium boiling pots. Consequently, the aim of the study was to design and fabricate an aluminium water boiling pot that incorporates internal cylindrical fins whose position/location are fractally generated using affine rules. A computer source codes that can generate arbitrary Iterated Fractal System (IFS) as well as their corresponding internal cylindrical fins placement locations on the bottom plate of the pot was also implemented.

2.0 Materials and Methods

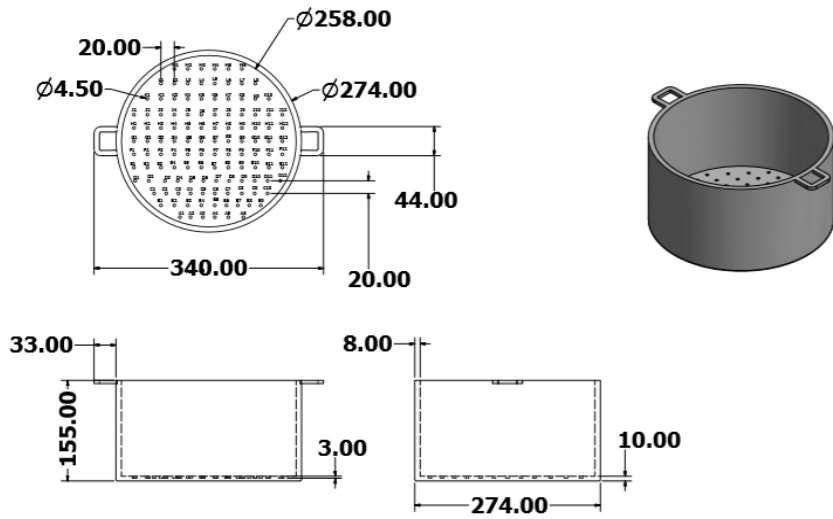
2.1 Materials

The materials used include aluminium wire and aluminium alloy. Aluminium wire was procured for the construction of the internal cylindrical fins. The EABP was produced by sand casting from aluminium alloy.

2.2 Design of the Experimental Aluminium Boiling Pot

A 7-litre EABP was designed and fabricated by sand casting using aluminium alloy. The detailed drawings of the experimental pot are shown in Figure 1.

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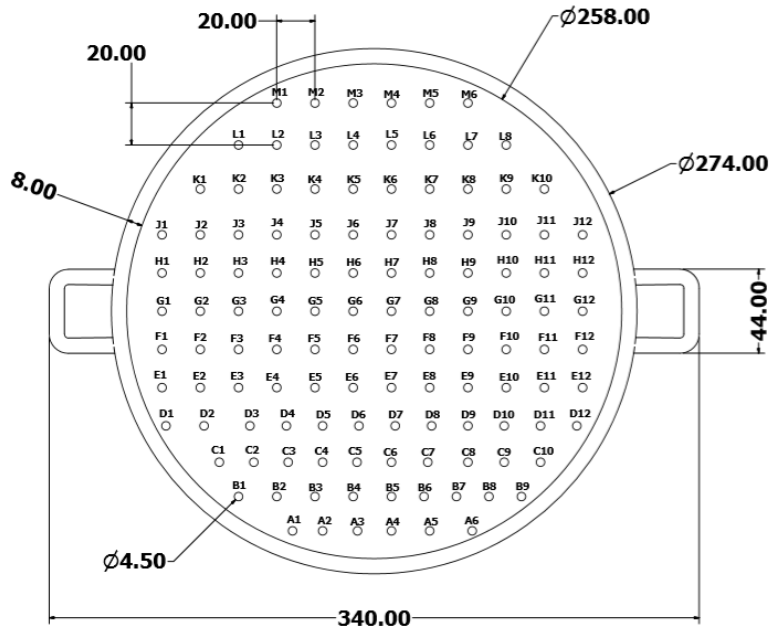
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Figure 1: EABP

2.3 Design of the Bottom Plate of the Experimental Aluminium Boiling Pot

The bottom plate of the EABP was divided into twenty four (24) grid lines at an equal interval of 10 mm along both horizontal and vertical axes. The coordinates of each of the formed points at 20 mm interval on both vertical (A, B, C...H, J, K, L, M) and horizontal (1, 2, 3..., 12) axes on the bottom plate of the pot were marked and properly labelled as shown in Figure 2. These formed points are one hundred and twenty one (121) in number and they are the potential fractal placement locations for the internal cylindrical fins. Holes of diameter $\text{Ø}4.5$ mm were drilled to a depth of 3 mm through the 121 potential fractal placement locations for the internal cylindrical fins heat transfer surfaces.

Preliminary investigation on the study revealed that better performance of the internal cylindrical fins can be achieved without causing the leakages of the pot when placed at fractal locations formed at 20 mm interval on both axes on the bottom plate of the pot.



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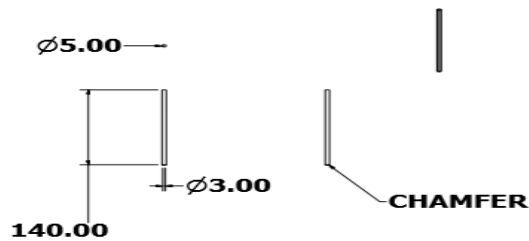
Figure 2: Bottom Plate of the EABP Showing the Internal Cylindrical Fins' Potential Placement Locations

The one hundred and twenty one potential fractal placement locations for the internal cylindrical fins are labelled from A1(8,2), A2(10,2), A3(12,2), A4(14,2), A5(16,2), A6(18,2), B1(6,4), B2(8,4), B3(10,4), B4(12,4), B5(14,4), B6(16,4), B7(18,4), B8(20,4), B9(22,4), C1(4,6), C2(6,6), C3(8,6), C4(10,6), C5(12,6), C6(14,6), C7(16,6), C8(18,6), C9(20,6), C10(22,6), D1(2,8), D2(4,8), D3(6,8), D4(8,8), D5(10,8), D6(12,8), D7(14,8), D8(16,8), D9(18,8), D10(20,8), D11(22,8), D12(24,8), E1(2,10), E2(4,10), E3(6,10), E4(8,10), E5(10,10), E6(12,10), E7(14,10), E8(16,10), E9(18,10), E10(20,10), E11(22,10), E12(24,10), F1(2,12), F2(4,12), F3(6,12), F4(8,12), F5(10,12), F6(12,12), F7(14,12), F8(16,12), F9(18,12), F10(20,12), F11(22,12), F12(24,12), G1(2,14), G2(4,14), G3(6,14), G4(8,14), G5(10,14), G6(12,14), G7(14,14), G8(16,14), G9(18,14), G10(20,14), G11(22,14), G12(24,14), H1(2,16), H2(4,16), H3(6,16), H4(8,16), H5(10,16), H6(12,16), H7(14,16), H8(16,16), H9(18,16), H10(20,16),

H11(22,16), H12(24,16), J1(2,18), J2(4,18), J3(6,18), J4(8,18), J5(10,18), J6(12,18), J7(14,18), J8(16,18), J9(18,18), J10(20,18), J11(22,18), J12(24,18), K1(4,20), K2(6,20), K3(8,20), K4(10,20), K5(12,20), K6(14,20), K7(16,20), K8(18,20), K9(20,20), K10(22,20), L1(6,22), L2(8,22), L3(10,22), L4(12,22), L5(14,22), L6(16,22), L7(18,20), L8(20,22), M1(8,24), M2(10,24), M3(12,24), M4(14,24), M5(16,24) and M6(18,24) respectively.

2.4 Design of Internal Cylindrical Fins

The heat transfer internal cylindrical fins were designed to be of equal dimension $\text{Ø}5 \times 140$ mm and chamfered at one end to diameter $\text{Ø}3$ mm in order to be comfortably fitted into any of the 121 placement locations on the bottom plate of the EABP. The one hundred and forty (140) millimetre length of the fins was selected in order to transfer heat to at least ninety percent (90 %) of the entire height of the pot when placed at the fractal fin locations on the bottom plate of the pot. Figure 3 shows the diagram of the heat transfer internal cylindrical fins.



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Figure 3: Internal Cylindrical Fin

2.5 Fabrication Procedures of the 7-Litre Experimental Aluminium Boiling Pot

Sand casting was used as the fabrication method of the EABP because of its simplicity and almost any material can be cast, no limit to size, shape or weight. The casting was carried out at the Foundry Unit of Olusegun Obasanjo Centre for Engineering Innovation, The Federal Polytechnic, Ado-Ekiti, Ekiti State, Nigeria. Ado-Ekiti is situated between longitude $05^{\circ} 06' 18''$

and 05°24' 00" East of the Greenwich Meridian and latitude 07° 32' 11" to 07°40' 28" North of the Equator (Aroge *et al.*, 2023). The basic steps taken are:

Step 1: Pattern Production

The pattern of the EABP was made from an existing pot. The pot was cut into two equal halves in order to form the two pieces of the pattern. The explicit drawing of the pattern is shown in Figure 4.

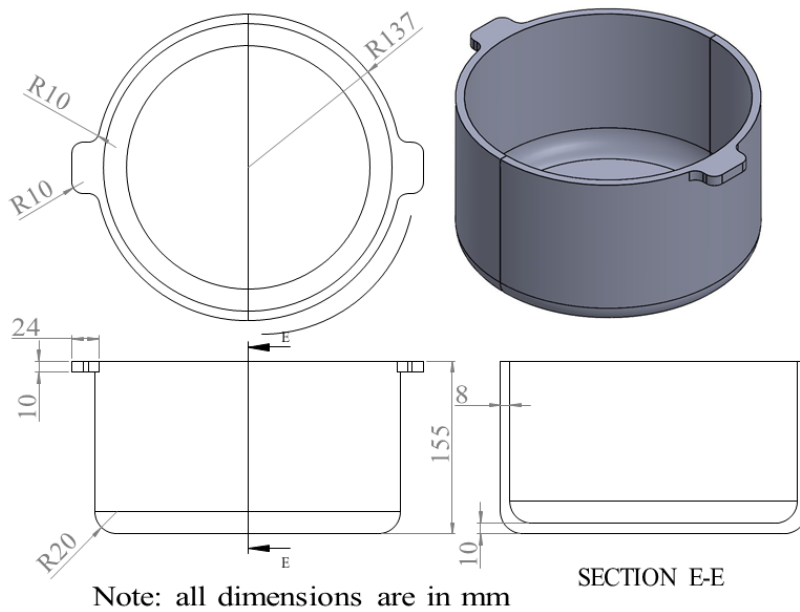
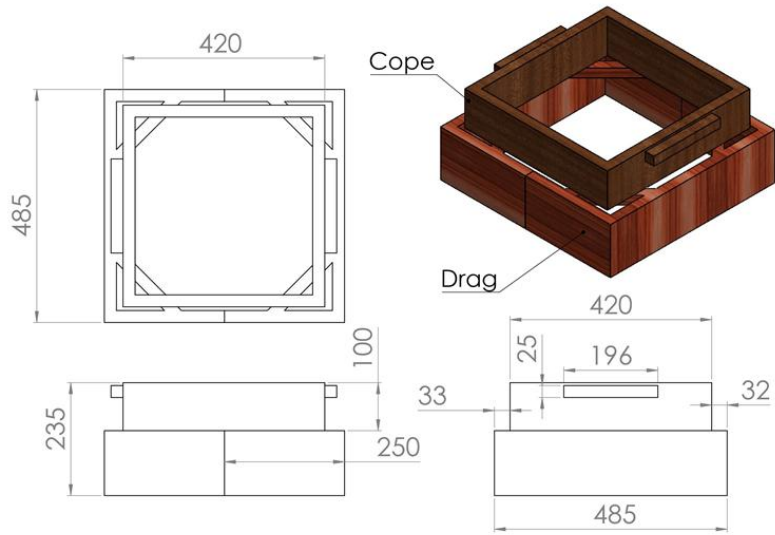


Figure 4: Pattern

Step 2: The moulding box consists of the drag and cope. It was made from wooden materials. The drag is the lower part of the moulding box and consists of two equal halves, while the upper part is called the cope. The flask which is the assembly of the drag and cope is shown in Figure 5.



Note: all dimensions are in mm

Figure 5: Flask

Step 3: The upper part of the moulding box called the cope is placed on the drag containing the pattern, filled with sand and gently hammered with provision made for the runner on top of the cope for the entrance of the molten metal as shown in Plate 1.



Plate 1: Assembly of Cope and Drag Showing the Runner.

Step 4: The cope and the two halves of the drag were disassembled in order to remove the pattern from the mould cavity as shown in Plate 2.



Plate 2: Dissembled Cope and Drag

Step 5: The cope and drag are assembled together while the molten metal is poured into the mould cavity through the runner. After pouring, the metal is left to cool and solidify. On completion, the sand moulds are removed from the flask and the cast aluminium pot knocked out while the removal of sharp edges of the cast aluminium pot was done by using grinding machine and the potential fractal placement locations of the internal cylindrical fins on the bottom plate of the pot were marked out and drilled accordingly.

2.6 Iterated Fractal System (IFS) Algorithms Computer Source Codes

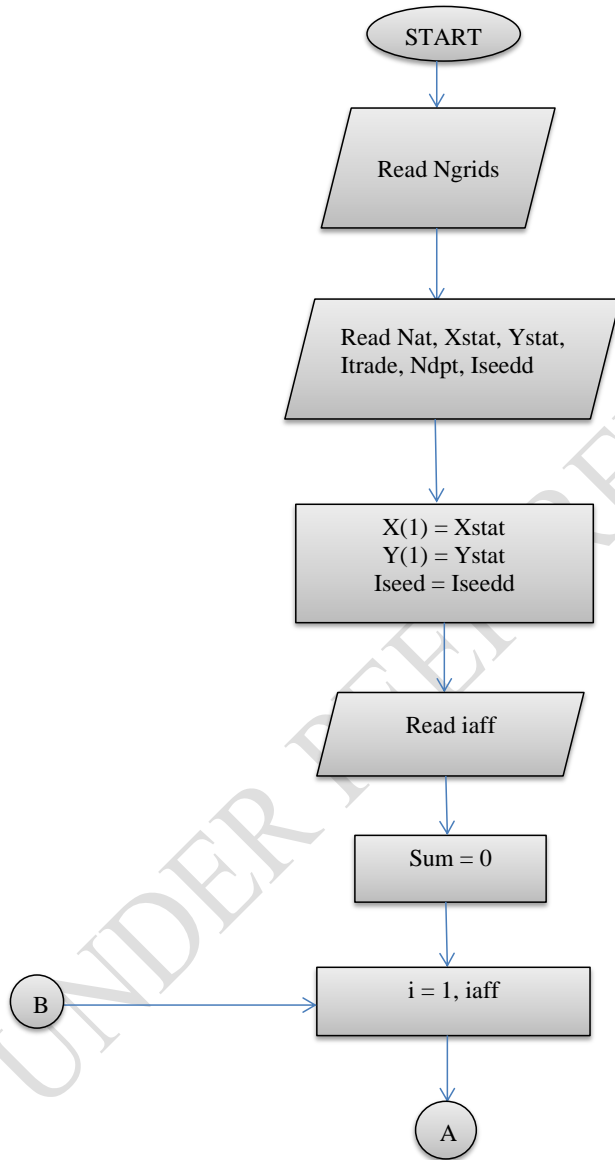
The IFS fractals can be obtained by playing ‘Chaos Game’ with their corresponding affine functions that are finite in number. According to Scheinerman (1996), affine functions are of the general form given by equation (1). Therefore a function ‘g’ is defined by specification of value for six numbers ‘a’ through ‘f’. Similarly and with respect to equation (1) a matrix ‘A’ and its corresponding determinant ‘DET’ can also be defined respectively as in equations (2) and (3). For this study, the IFS based algorithms computer source codes for the generation of arbitrary

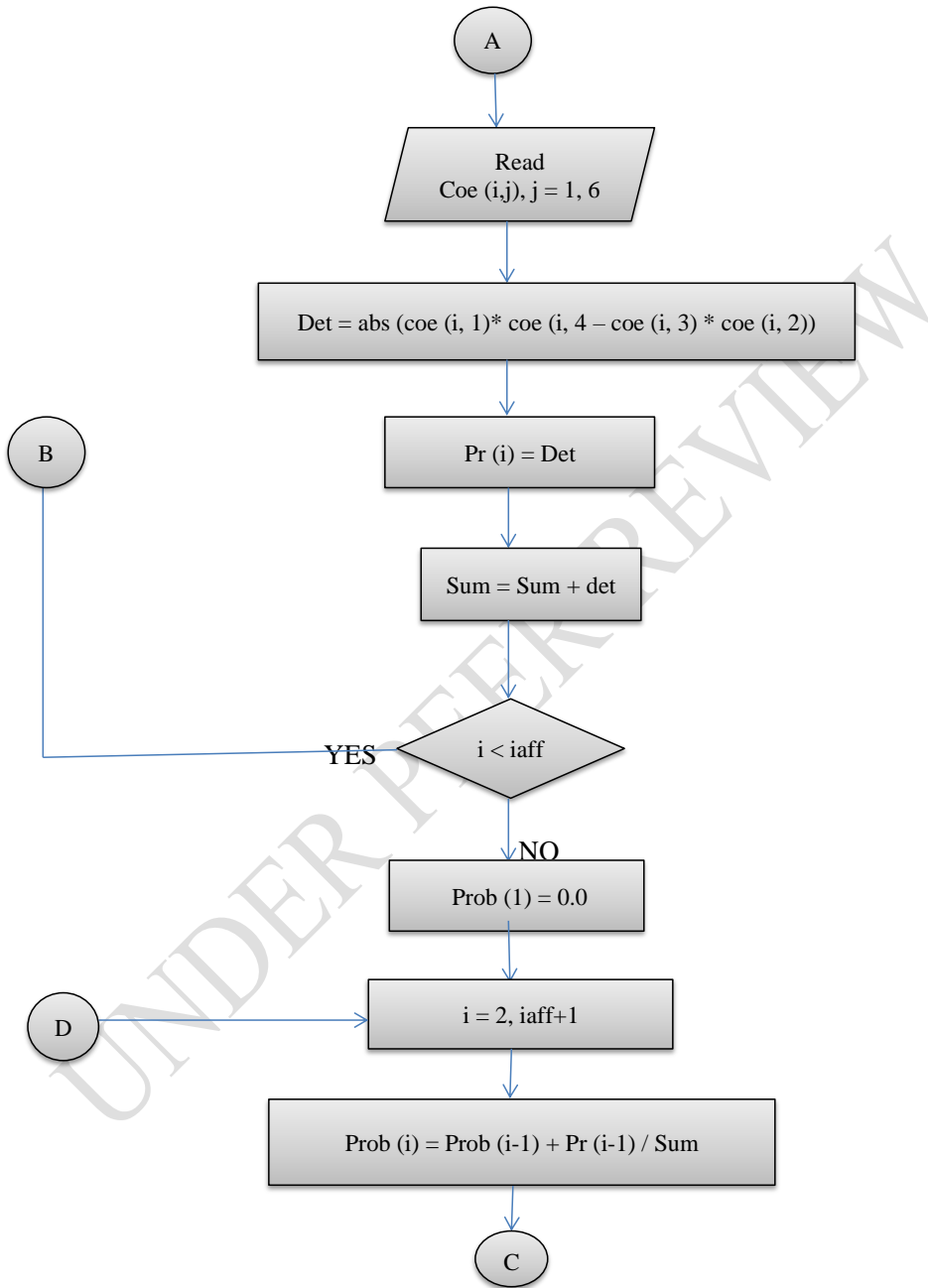
selected fractal objects and their corresponding internal cylindrical fins' placement locations on the bottom plate of the pot were illustrated by the flowchart in Figure 6. The flowchart derived its strength from equations (1) to (3) for finite affine functions called 'Iaff' to play the 'Chaos Game' and obtain 2-dimensional Cartesian coordinate solutions of associated arbitrary IFS fractal. The solutions were thereafter transformed to potential cylindrical fin locations from which locations for number experimental fins are selected on first appearance basis.

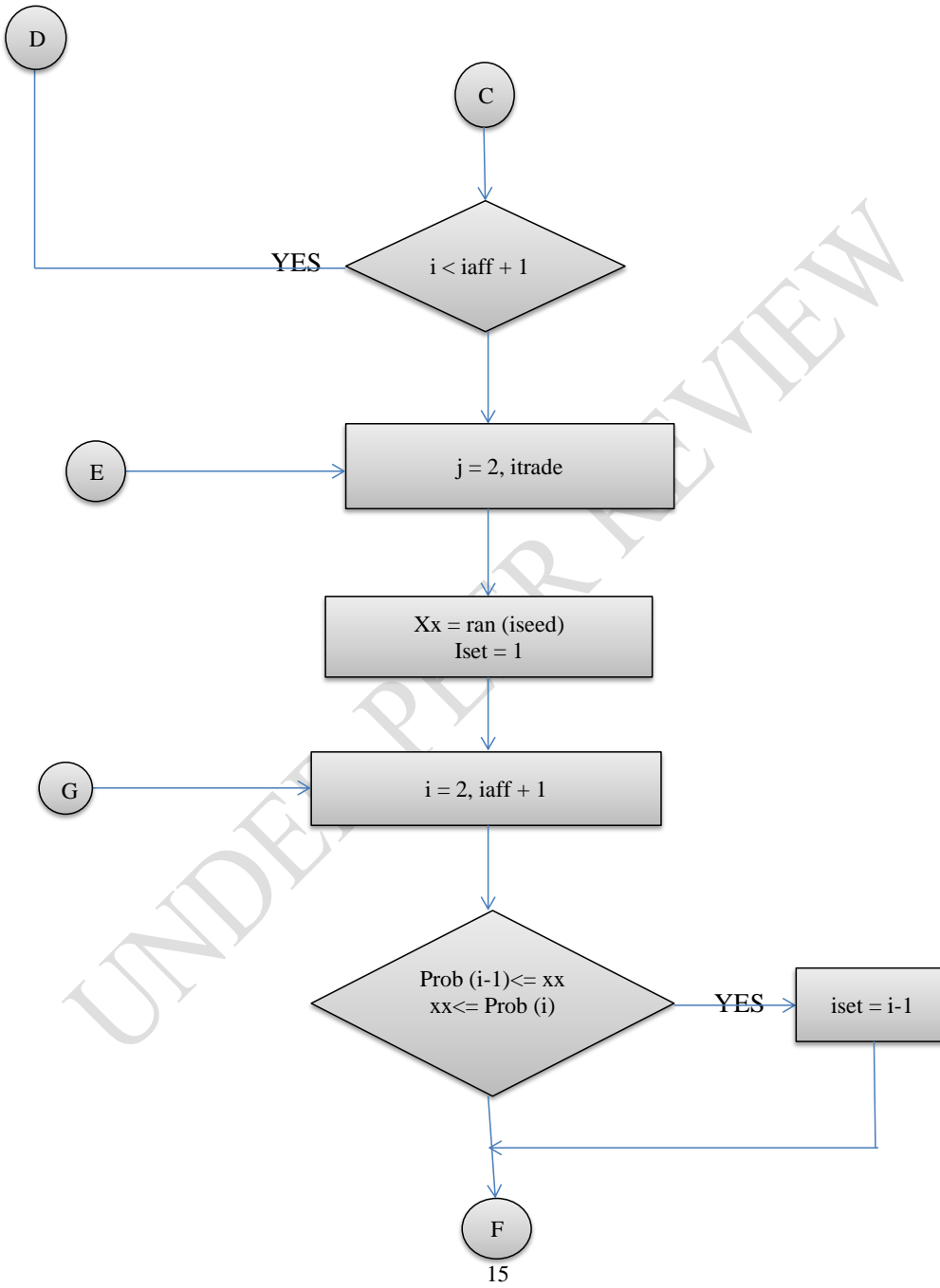
$$g \begin{bmatrix} x \\ y \end{bmatrix} = \begin{bmatrix} a & b \\ c & d \end{bmatrix} \begin{bmatrix} x \\ y \end{bmatrix} + \begin{bmatrix} e \\ f \end{bmatrix} \quad (1)$$

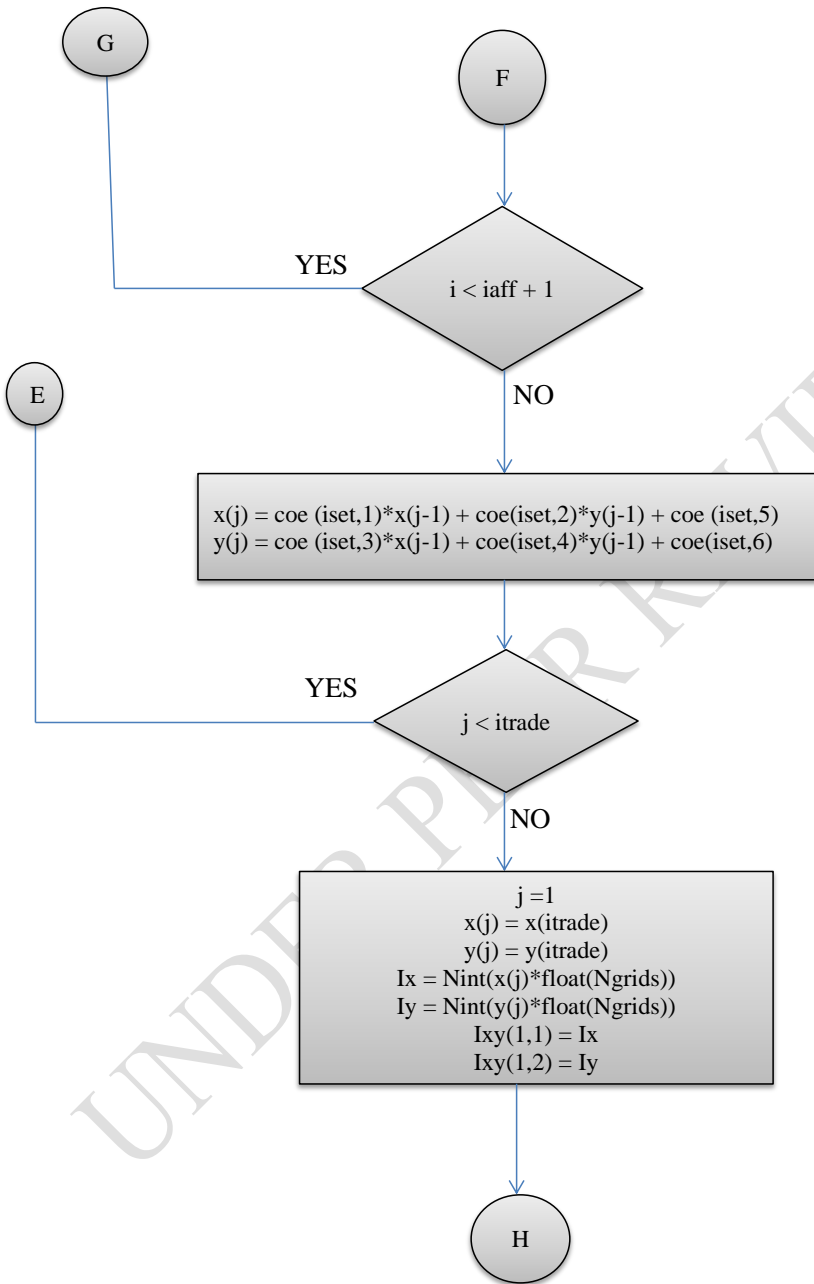
$$A = \begin{bmatrix} a & b \\ c & d \end{bmatrix} \quad (2)$$

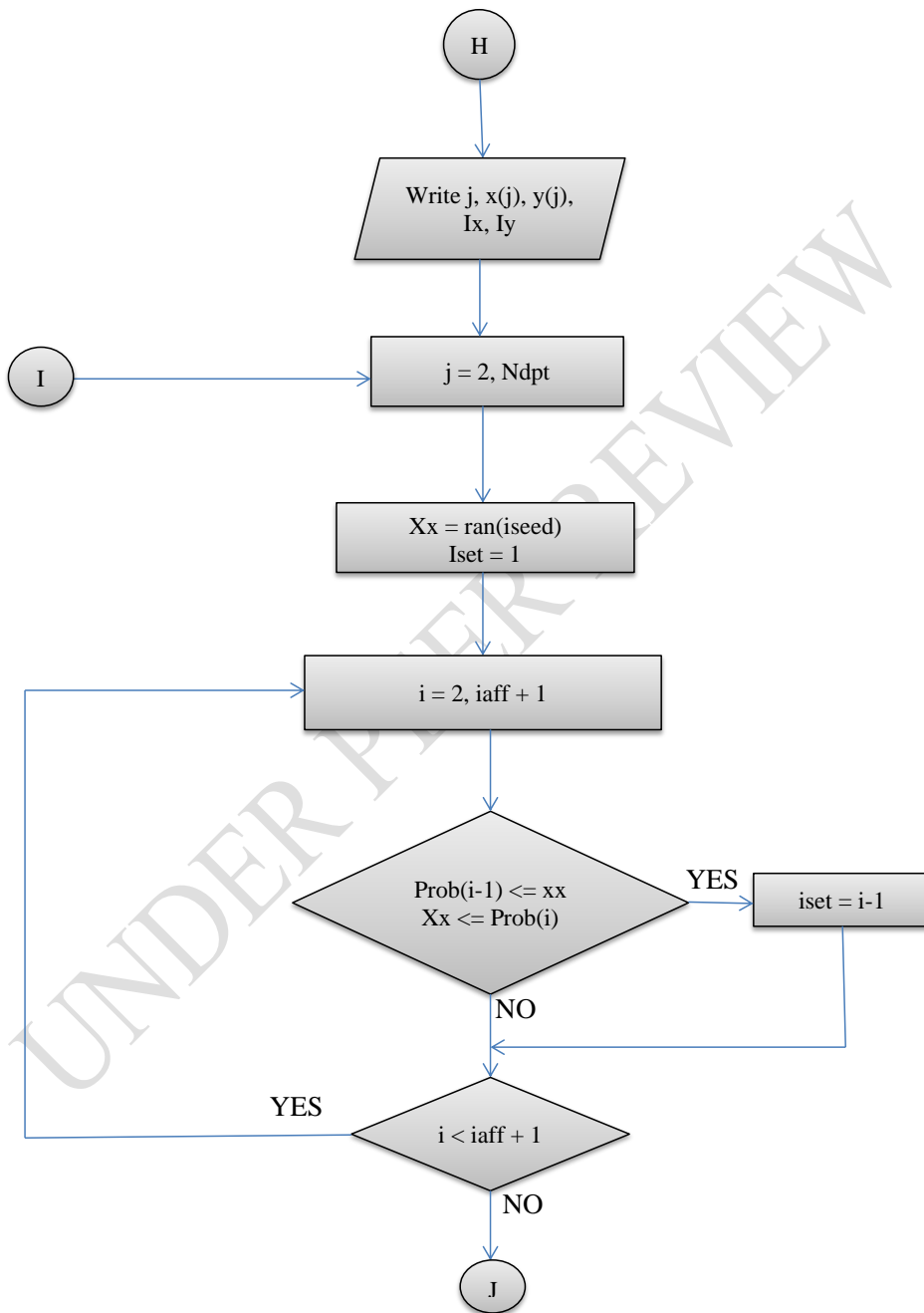
$$DET = |A| = \begin{vmatrix} a & b \\ c & d \end{vmatrix} \quad (3)$$

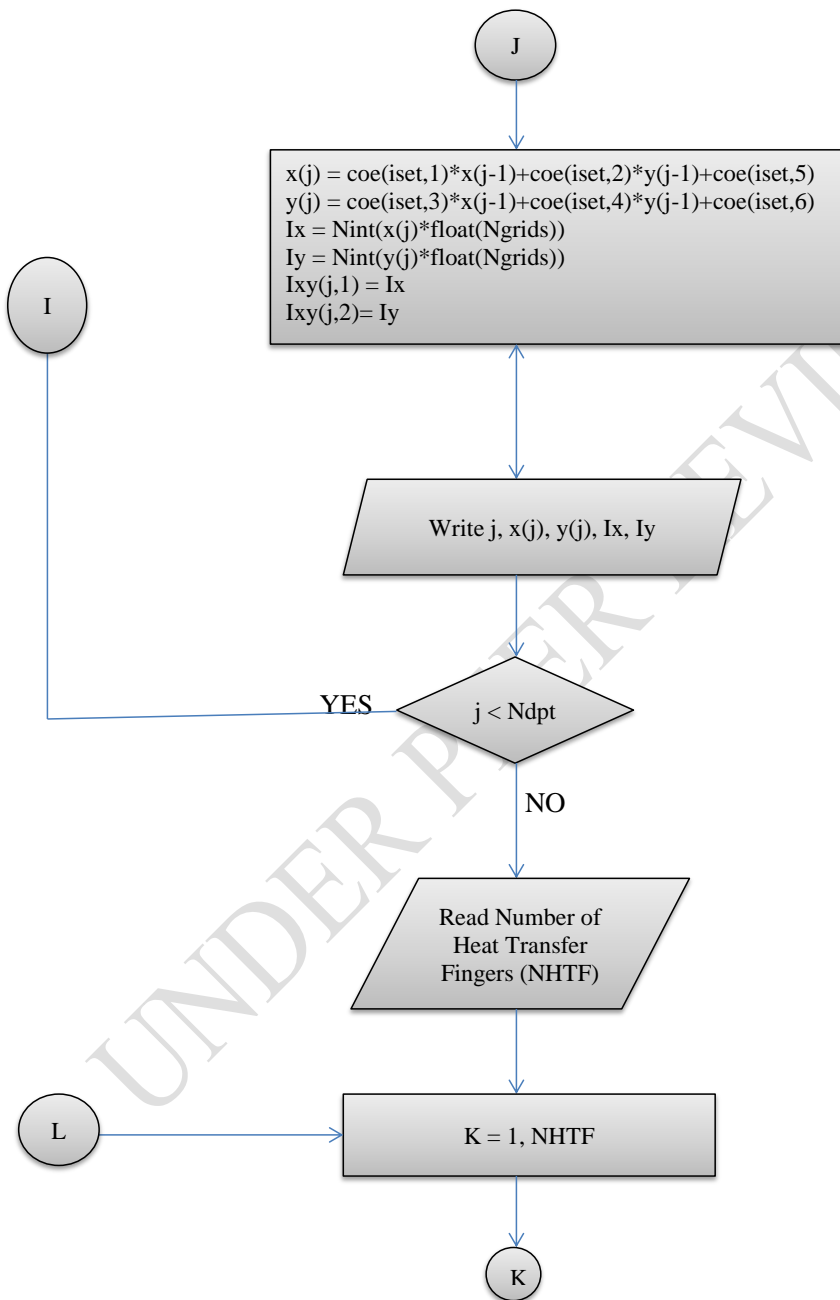












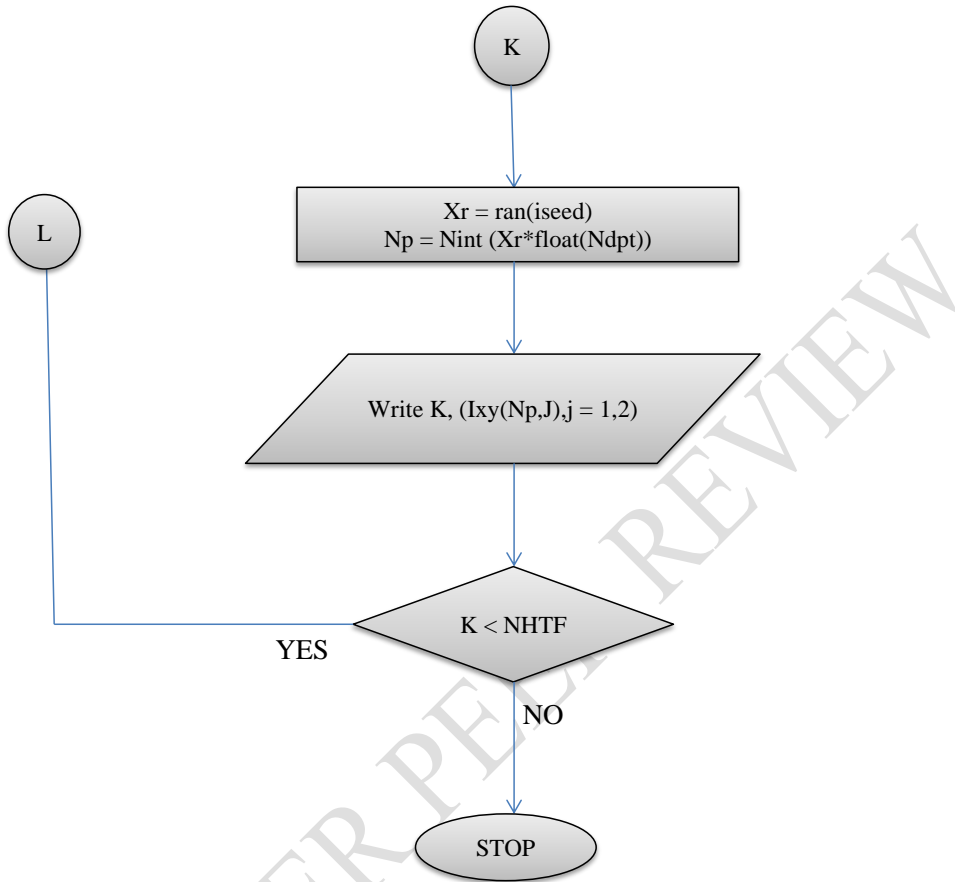


Figure 6: The Selected Fractal Objects Algorithms/ Flowchart

The chaos game based algorithms computer source codes illustrated in the flowchart can generate arbitrary IFS fractal objects such as Koch Curve, Xmas Tree, Triangle, Fractal-L and Fractal-T among others and their corresponding internal cylindrical fins' placement locations on the bottom plate of the fabricated experimental aluminium boiling pot.

2.7 Formation of Experimental Aluminium Boiling Pot Incorporated with Internal Cylindrical Fins.

Experimental Aluminium Boiling Pots denoted by EABP3, EABP5, EABP7 and EABP9 were obtained by placing 3, 5, 7 and 9 internal cylindrical fins, respectively, on the bottom plate of the

experimental pot at placement locations determined by arbitrarily selected generated IFS fractal objects.

3.0 Results and Discussion

3.1 The Fabricated 7-litre Experimental Aluminium Boiling Pot and Internal Cylindrical Fins.

The fabricated 7-litre EABP is shown in Plate 3. The pot weighs 3348 g. It has base thickness, height, internal diameter and external diameter of 10, 155, 258 and 274 mm, respectively. Also, the EABP was produced with a feature of one hundred and twenty one (121) placement locations for the internal cylindrical fins as shown in Plate 4.

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Plate 3: 7-litre EABPs



Plate 4: 7-litre EABPs Showing the Internal Cylindrical Fins' Potential Placement Locations

The fabricated internal cylindrical fins are shown in Plate 5.



Plate 5: Heat Transfer Internal Cylindrical Fins ($\text{Ø}5 \times 140 \text{ mm}$)

The aluminium alloy and aluminium wire used for the fabrication of the EABP and internal cylindrical fins were characterised to be 73.3405 and 77.7118 % aluminium as shown in Table 1 and 2, respectively, by the National Agency for Science and Engineering Infrastructure (NASeni), Km 4, Ondo Road, Akure, Ondo State, Nigeria. Akure is located between latitude $7^{\circ}17' \text{ N}$ and longitude $5^{\circ}4' \text{ E}$ (Olajuyigbe *et al.*, 2016).

Table 1: Aluminium Alloy Chemical Composition

Element	Percentage Content
Mg	6.8335
Al	73.3405
Si	10.7221
Ti	0.3866
Cr	0.0063
Mn	0.1521
Fe	2.1653
Ni	0.2376
Cu	2.6693
Zn	1.8809
Sr	0.0122
Pb	0.0921
Sn	0.5486
Sb	0.9429

Table 2: Aluminium Wire Chemical Composition

Element	Percentage Content
Mg	5.3592
Al	77.7118
Si	13.8980
Ti	0.0000
Cr	0.0066
Mn	0.0322
Fe	1.1126
Ni	0.0385
Cu	0.0000
Zn	0.2364
Sr	0.0060
Pb	0.0000
Sn	0.4793
Sb	1.1092

3.2 Fabricated Experimental Aluminium Boiling Pot Incorporated with Internal Cylindrical Fins

Some of the EABPs formed by placing 3 and 5-internal cylindrical fins on the bottom plate of the pot using Xmas Tree affine rule respectively are shown in Plates 6 and 7.



Plate 6: The EABP Incorporated with Xmas Tree Rule Using 3-Internal Cylindrical Fins



Plate 7: The EABP Incorporated with Xmas Tree Rule Using 5-Internal Cylindrical Fins

4.0 Conclusion

In this study, a novel water boiling pot was successfully developed. This pot has a feature that can accommodate internal cylindrical fins whose placement locations were determined by Iterated Fractal System that are generated using chaos game method. The fins are capable of improving the boiling pot performance when compared to traditional water boiling pot in terms of shortest boiling time as well as fuel consumption.

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COMPETING INTERESTS DISCLAIMER:

Authors have declared that they have no known competing financial interests OR non-financial interests OR personal relationships that could have appeared to influence the work reported in this paper.

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